

## Phase Relationships Involving Mixed $O'$ - $\beta'$ Sialons in the Y-Si-Al-O-N System

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### SUMMARY

*As a preliminary to investigating  $O'$ - $\beta'$  phase relationships in the Y-Si-Al-O-N system, sub-solidus phase relationships in the  $Si_2N_2O$ -AlN- $Y_2O_3$  system have been studied. The results show that two AlN-containing triangles and eight tetrahedra, of which seven contain YAG, occur in this system, namely:  $Y_2O_3$ -J-AlN; J-K-AlN; H- $Si_3N_4$ - $O'_{ss}$ - $Si_2N_2O$ ; K- $Si_3N_4$ -H-YAG; K- $Si_3N_4$ -AlN-YAG; H- $Si_3N_4$ - $O'_{ss}$ -YAG;  $Si_3N_4$ - $O'_{ss}$ - $\beta'$  ( $z=0.8$ )-YAG;  $O'_{ss}$ - $\beta'$  ( $z=0.8$ )-X-YAG; X- $\beta'$  ( $z=0.8$ )- $\beta'$  ( $z=4$ )-YAG;  $Si_3N_4$ - $\beta'$  ( $z=4$ )-AlN-YAG.*

*Phase relationships involving  $O'$ - $\beta'$  sialon in the Y-Si-Al-O-N system have been revised. In the Si-Al-O-N system, the  $O'$ - $\beta'$  two-phase region consists of two compatibility triangles:  $Si_3N_4$ - $Si_2N_2O$ - $O'_{ss}$  ( $x=0.3$ ) and  $Si_3N_4$ - $\beta'$  ( $z=0.8$ )- $O'_{ss}$  ( $x=0.3$ ). In the Y-Si-Al-O-N system, there are three compatibility tetrahedra involved in the  $O'$ - $\beta'$  region, and the sub-solidus phase relationships depend on temperature. At 1550°C, these three compatibility tetrahedra are  $Si_3N_4$ - $Si_2N_2O$ - $O'_{ss}$  ( $x=0.3$ )-H,  $Si_3N_4$ - $O'_{ss}$  ( $x=0.3$ )-H-YAG and  $Si_3N_4$ - $\beta'$  ( $z=0.8$ )- $O'_{ss}$  ( $x=0.3$ )-YAG. At devitrification temperatures (1200-1300°C), they are:  $Si_3N_4$ - $Si_2N_2O$ - $O'_{ss}$  ( $x=0.3$ )- $Y_2Si_2O_7$ ,  $Si_3N_4$ - $O'_{ss}$  ( $x=0.3$ )- $Y_2Si_2O_7$ -YAG and  $Si_3N_4$ - $\beta'$  ( $z=0.8$ )- $O'_{ss}$  ( $x=0.3$ )-YAG.*

### 1 INTRODUCTION

In recent years two-phase ceramics have received more and more attention, since they offer the advantage over single phase materials that their

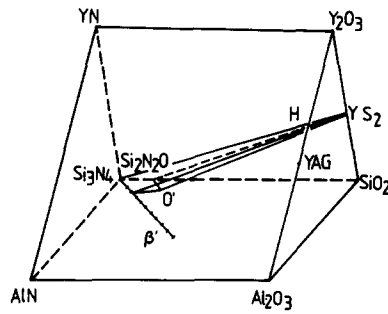


Fig. 1. The compatibility pyramid  $\text{Si}_3\text{N}_4\text{-Si}_2\text{N}_2\text{O-}\beta'(z=0.8)\text{-O}'_{\text{ss}}\text{-Y}_2\text{Si}_2\text{O}_7$  from Naik *et al.*<sup>4</sup>  $\text{YAG} = 3\text{Y}_2\text{O}_3 \cdot 5\text{Al}_2\text{O}_3$ ,  $\text{YS}_2 = \text{Y}_2\text{Si}_2\text{O}_7$ ,  $\text{H} = \text{Y}_{10}(\text{SiO}_4)_6\text{N}_2$ .

properties can be tailored extensively.  $\beta'$ -Sialon has already been established as a good high-temperature engineering ceramic with excellent mechanical properties.  $\text{O}'$ -Sialon ( $\text{Si}_2\text{N}_2\text{O}$ )<sub>ss</sub> ceramics either hot-pressed<sup>1</sup> or pressureless sintered<sup>2</sup> possess good oxidation resistance up to 1350–1400°C.  $\text{O}'$ - $\beta'$  composite sialons offer good prospects for development as ceramic materials, combining the mechanical properties of  $\beta'$  with the good oxidation resistance of  $\text{O}'$ . Dense  $\text{O}'$ - $\beta'$  sialons<sup>3</sup> have been fabricated by pressureless sintering using  $\text{Y}_2\text{O}_3$  as an additive. Most of the intergranular glassy phase can be devitrified to produce  $\text{Y}_2\text{Si}_2\text{O}_7$  and YAG by sequential

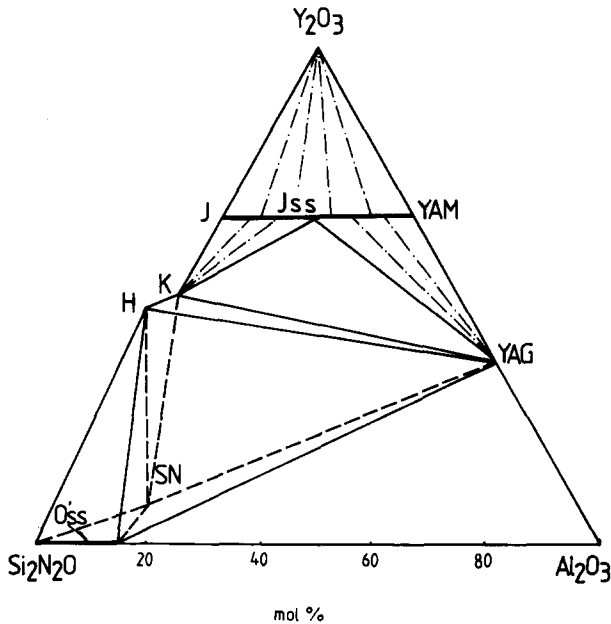


Fig. 2. Sub-solidus diagram of the  $\text{Si}_2\text{N}_2\text{O-Al}_2\text{O}_3\text{-Y}_2\text{O}_3$  system from Cao *et al.*<sup>5</sup>  $\text{J} = 2\text{Y}_2\text{O}_3 \cdot \text{Si}_2\text{N}_2\text{O}$ ;  $\text{K} = \text{Y}_2\text{O}_3 \cdot \text{Si}_2\text{N}_2\text{O}$ ;  $\text{SN} = \text{Si}_3\text{N}_4$ ;  $\text{YAM} = 2\text{Y}_2\text{O}_3 \cdot \text{Al}_2\text{O}_3$ .

heat treatments and the oxidation resistance of the devitrified specimens is good up to at least 1300°C.

The crystalline products from the intergranular glass are determined by phase relationships. Previous phase relationships<sup>4</sup> show that  $O'-\beta'$  and  $Y_2Si_2O_7$  form a compatibility region, as shown in Fig. 1. However, Cao's work<sup>5</sup> on phase relations in the  $Si_2N_2O-Al_2O_3-Y_2O_3$  system indicates that  $O'$ -sialon should be in equilibrium with YAG and also with  $Si_3N_4$  and H-phase, as shown in Fig. 2. The present paper attempts to clear up this confusion.

The  $Si_2N_2O-AlN-Y_2O_3$  plane is considered to be mainly concerned with phase relationships involving  $O'-\beta'$  sialons. Like  $\beta'$ -sialon which can be synthesized from AlN and  $SiO_2$ ,<sup>6</sup>  $O'-\beta'$  composite sialons can also be produced by reacting AlN and  $Si_2N_2O$ . For these reasons phase relationships in the  $Si_2N_2O-AlN-Y_2O_3$  system were studied, and also taken as a continuation of our previous work on phase equilibrium studies in the  $Si_2N_2O$ -containing system.<sup>5</sup>

## 2 EXPERIMENTAL

Aluminium nitride, as one of the starting materials, was prepared in our laboratory, and contained 1.4% oxygen. The details of other starting powders used and preparation of specimens are the same as described in our previous paper.<sup>5</sup> The hot-pressing temperature used was 1700–1750°C for the compositions on the line joining  $Si_2N_2O$  and AlN, and 1600°C for ternary  $Y_2O_3$ -containing compositions. The phase compositions of the specimens after hot-pressing were determined by X-ray diffraction analysis.

## 3 RESULTS AND DISCUSSION

### 3.1 Phase relationships in the $Si_2N_2O-AlN$ system

As shown in the  $Si-Al-O-N$  phase diagram of Fig. 3,  $Si_2N_2O$ ,  $O'_{ss}$ ,  $Si_3N_4$  and  $\beta'_{ss}$  form a compatibility region. The solubility limit of  $Al_2O_3$  in  $Si_2N_2O$  was determined to be 15 mol/% (i.e.  $x = 0.3$  in the formula  $Si_{2-x}Al_xN_{2-x}O_{1+x}$ ).<sup>5</sup> The upper limit of  $\beta'$ -sialon coexisting with  $O'_{ss}$  was detected to be  $z = 0.8$  in the formula  $Si_{6-z}Al_zO_zN_{8-z}$ .<sup>3</sup> Our previous work<sup>5</sup> shows there should be a tie line joining  $O'_{ss}(x = 0.3)$  to  $Si_3N_4$ . Therefore the  $Si_2N_2O-AlN$  join would cut across four tie lines:  $Si_3N_4-O'_{ss}$ ,  $\beta'(z = 0.8)-O'_{ss}$ ,  $\beta'(z = 0.8)-x$  and  $Si_3N_4-\beta'(z = 4)$  at  $Si_2N_2O:AlN$  mol ratios of 4:3:1, 3:1, 1.6:1 and 1:1 respectively, forming five different phase regions:  $Si_2N_2O-O'_{ss}-Si_3N_4$ ,  $Si_3N_4-O'_{ss}-\beta'(z = 0.8)$ ,  $O'_{ss}-\beta'(z = 0.8)-x$ ,  $x-\beta'(z = 0.8)-\beta'(z = 2)$  and  $\beta'(z = 2)-AlN$  (and

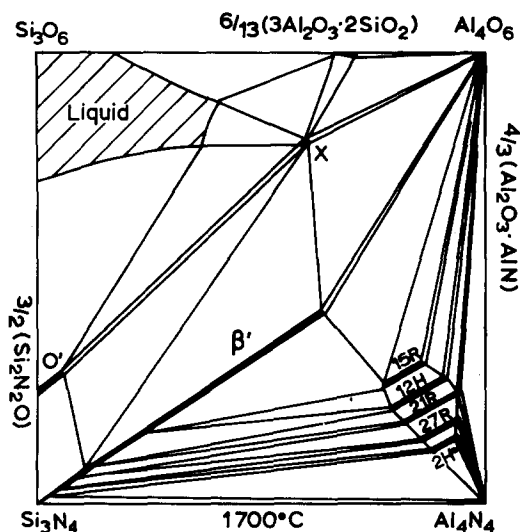
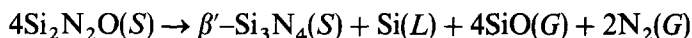


Fig. 3. Phase relationships in the  $\text{Si}_3\text{N}_4$ - $\text{SiO}_2$ - $\text{Al}_2\text{O}_3$ - $\text{AlN}$  system at  $1700^\circ\text{C}$  after Thompson *et al.*<sup>8</sup>

polytypes). The present work using  $\text{Si}_2\text{N}_2\text{O}$  and  $\text{AlN}$  as starting materials has confirmed the existence of these phase regions. The temperature used was  $1700$ – $1750^\circ\text{C}$ , since above  $1750^\circ\text{C}$  the decomposition of  $\text{Si}_2\text{N}_2\text{O}$  occurs according to the reaction:

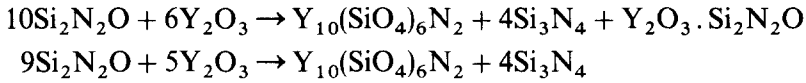


Compositions between  $\text{Si}_2\text{N}_2\text{O}$  and  $4:3 \text{Si}_2\text{N}_2\text{O}:\text{AlN}$  contain  $\text{Si}_2\text{N}_2\text{O}$  (and/or  $\text{O}'_{\text{ss}}$ ) and  $\beta'\text{-Si}_3\text{N}_4$  (with small amounts of  $\alpha\text{-Si}_3\text{N}_4$ ). Pure  $\beta'$  ( $z=2$ ) can be obtained at the  $\text{Si}_2\text{N}_2\text{O}:\text{AlN}$  composition at  $1750^\circ\text{C}$  but below this temperature the reaction is not complete. The compositions between  $\text{Si}_2\text{N}_2\text{O}:\text{AlN}$  and  $\text{AlN}$  give  $\beta'$  ( $z=2$ ) and  $\text{AlN}$  with a little 15R. The appearance of  $\text{AlN}$  instead of polytypes is expected, since the temperature used was not high enough to produce polytypes which are generally formed at above  $1800^\circ\text{C}$  if no or only a little liquid phase is present. The above results indicate that  $\text{O}'\text{-}\beta'$  sialon and  $\beta'$  ( $z=2$ ) can be synthesized from  $\text{Si}_2\text{N}_2\text{O}$  and  $\text{AlN}$  mixtures.

### 3.2 Phase relationships in two $\text{Y}_2\text{O}_3$ -containing binary systems

The two systems  $\text{Y}_2\text{O}_3\text{-Si}_2\text{N}_2\text{O}$  and  $\text{Y}_2\text{O}_3\text{-AlN}$  have been studied in our previous work<sup>5,7</sup> and it is unnecessary to repeat them. In the  $\text{Y}_2\text{O}_3\text{-Si}_2\text{N}_2\text{O}$  system, there are two compounds  $2\text{Y}_2\text{O}_3 \cdot \text{Si}_2\text{N}_2\text{O}(\text{J})$  and  $\text{Y}_2\text{O}_3 \cdot \text{Si}_2\text{N}_2\text{O}(\text{K})$ , as shown in Fig. 2. At the  $\text{Si}_2\text{N}_2\text{O}$ -rich corner,  $\text{Si}_2\text{N}_2\text{O}$  reacts at  $1550^\circ\text{C}$  with

Y<sub>2</sub>O<sub>3</sub> to form Y<sub>10</sub>(SiO<sub>4</sub>)<sub>6</sub>N<sub>2</sub>(H) and Si<sub>3</sub>N<sub>4</sub> (mainly α-form, with a little β) by the following reactions:

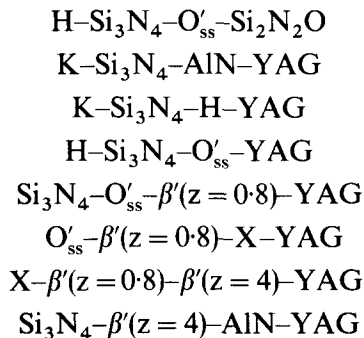


The existence of the compatibility region Si<sub>2</sub>N<sub>2</sub>O-O'<sub>ss</sub>-Si<sub>3</sub>N<sub>4</sub>-h is contrary to other authors' results. The contradiction is caused mainly by the different experimental conditions used. Our previous work shows that H-phase completely disappears above 1700°C to form the glassy phase which can be devitrified to give Y<sub>2</sub>Si<sub>2</sub>O<sub>7</sub>. The fact that different products are obtained by different experimental conditions emphasizes the point that sub-solidus phase relationships are not temperature invariant.

The system Y<sub>2</sub>O<sub>3</sub>-AlN does not produce any quaternary compounds.

### 3.3 Sub-solidus phase relationships in the Si<sub>2</sub>N<sub>2</sub>O-AlN-Y<sub>2</sub>O<sub>3</sub> system

The temperature used inside the triangle was 1600°C which did not give any liquid in the compositions explored. The results obtained were used to construct the phase diagrams shown in Figs 4-6. Within this system, there exists two AlN-containing compatibility triangles J-Y<sub>2</sub>O<sub>3</sub>-AlN and K-J-AlN. In the Si<sub>2</sub>N<sub>2</sub>O-rich area, the phase relationships are rather complicated; K, H, Si<sub>3</sub>N<sub>4</sub>, O'<sub>ss</sub> (x = 0.3), β'<sub>ss</sub> and AlN are all compatible with YAG, thus forming seven YAG-containing compatibility tetrahedra. Altogether there exist eight tetrahedra involved in this system:



The results obtained are in good agreement with our previous work,<sup>5</sup> but contrary to the phase relationships obtained by Naik *et al.*<sup>4</sup> who reported the whole Si<sub>3</sub>N<sub>4</sub>-Si<sub>2</sub>N<sub>2</sub>O-O'<sub>ss</sub>-β'(z = 0.8) region to be coexisting with Y<sub>2</sub>Si<sub>2</sub>O<sub>7</sub>, as shown in Fig. 1. The determination of phase relationships of this ternary system is beneficial for the fabrication of O'-β' composite ceramics from Si<sub>2</sub>N<sub>2</sub>O and AlN using Y<sub>2</sub>O<sub>3</sub> as an additive.

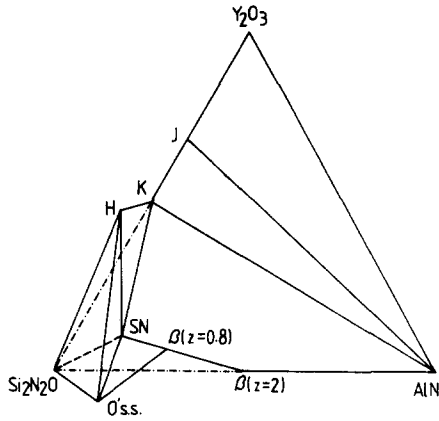


Fig. 4. Sub-solidus diagram of the  $\text{Si}_2\text{N}_2\text{O}-\text{AlN}-\text{Y}_2\text{O}_3$  system.

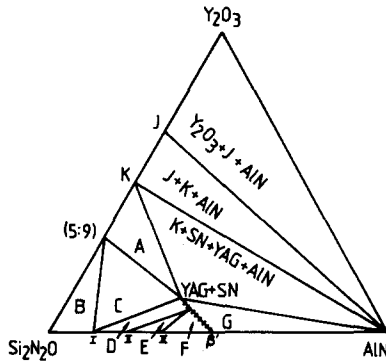


Fig. 5. Sub-solidus diagram of the  $\text{Si}_2\text{N}_2\text{O}-\text{AlN}-\text{Y}_2\text{O}_3$  system.  $\text{I} = \text{O}'_{\text{ss}} + \text{Si}_3\text{N}_4$ ;  $\text{II} = \text{O}'_{\text{ss}} + \beta'(z=0.8)$ ;  $\text{III} = \beta'(z=0.8) + x$ ;  $(5:9) = \text{H} + \text{Si}_3\text{N}_4$ ;  $\text{A} = \text{K} + \text{H} + \text{Si}_3\text{N}_4 + \text{YAG}$ ;  $\text{B} = \text{H} + \text{Si}_3\text{N}_4 + \text{Si}_2\text{N}_2\text{O} + \text{O}'_{\text{ss}}$ ;  $\text{C} = \text{H} + \text{Si}_3\text{N}_4 + \text{O}'_{\text{ss}} + \text{YAG}$ ;  $\text{D} = \text{Si}_3\text{N}_4 + \text{O}'_{\text{ss}} + \beta'(z=0.8) + \text{YAG}$ ;  $\text{E} = \text{O}'_{\text{ss}} + \beta'(z=0.8) + \text{X} + \text{YAG}$ ;  $\text{F} = \text{X} + \beta'(z=0.8) + \beta'(z=4) + \text{YAG}$ ;  $\text{G} = \text{Si}_3\text{N}_4 + \beta'(z=4) + \text{AlN} + \text{YAG}$ .

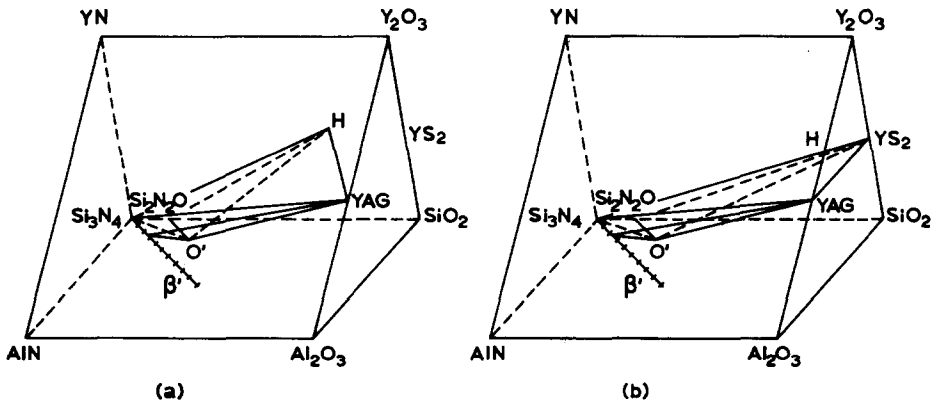
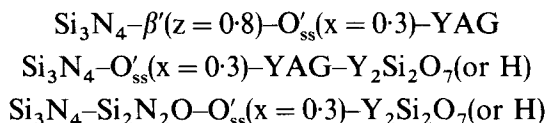


Fig. 6. Phase relationships of  $\text{O}'-\beta'$ -sialon in  $\text{Y}-\text{Si}-\text{Al}-\text{O}-\text{N}$  system (a) at  $1550^\circ\text{C}$ , (b) at devitrifying temperatures  $1200-1300^\circ\text{C}$ .

### 3.4 Phase relationships involving O'-β' sialon in the Y-Si-Al-O-N system

O'-β' Phase relationships can be summarized as follows:



The two triangles  $\text{Si}_3\text{N}_4-\text{Si}_2\text{N}_2\text{O}-\text{O}'_{\text{ss}}(x=0.3)$  and  $\text{Si}_3\text{N}_4-\text{O}'_{\text{ss}}(x=0.3)-\text{YAG}$  at lower temperatures (about 1550°C) join to H-phase. At higher temperatures (about 1700°C) H-phase dissolves into liquid phase and  $\text{Y}_2\text{Si}_2\text{O}_7$  can then be crystallized from the liquid if sequential heat treatment is used. So the phase relationships of O'-β' sialon are temperature dependent. For the fabrication of dense O'-β' sialon ceramics, the temperature used for sintering is usually above 1700°C and  $\text{Y}_2\text{Si}_2\text{O}_7$  is expected to be the intergranular crystalline phase instead of H-phase. The revised phase relationships can satisfactorily explain the appearance of YAG in O'-β' sialon ceramics<sup>3</sup> and indicated that there is a choice of either  $\text{Y}_2\text{Si}_2\text{O}_7$ , YAG or both of these as grain-boundary phases for O'-β' sialons.

## 4 CONCLUSIONS

- (1) The sub-solidus phase diagram of the  $\text{Si}_2\text{N}_2\text{O}-\text{AlN}-\text{Y}_2\text{O}_3$  is presented. Within this system no new compound has been found but two ternary phase regions and eight quaternary tetrahedra are identified.
- (2) Phase relationships involving O'-β' sialons in the Y-Si-Al-O-N system have been revised. The phase relationships are temperature dependent. Three compatibility tetrahedra,  $\text{Si}_3\text{N}_4-\text{Si}_2\text{N}_2\text{O}-\text{O}'_{\text{ss}}-\text{Y}_2\text{Si}_2\text{O}_7$  (or H),  $\text{Si}_3\text{N}_4-\text{O}'_{\text{ss}}-\beta'(z=0.8)-\text{YAG}$  and  $\text{O}'_{\text{ss}}-\text{Si}_3\text{N}_4-\text{YAG}-\text{Y}_2\text{Si}_2\text{O}_7(\text{or H})$  have been found.

## REFERENCES

1. Huang, Z. K., Greil, P. and Petzow, G., Formation of Silicon Oxynitride from  $\text{Si}_3\text{N}_4$  and  $\text{SiO}_2$  in the Presence of  $\text{Al}_2\text{O}_3$ , *Ceramics International*, **10**(1) (1984) 14-17.
2. Trigg, M. B. and Jack, K. H., Silicon Oxynitride and O'-Sialon Ceramics, In: *Proc. First Int. Symp. on Ceramic Components for Engines, 1983 Hakone, Japan*, Eds S. Somiya, E. Kanai and K. Ands, KTK Scientific Publishers, Japan, 1984, 199-217.
3. Sun, W. Y., Thompson, D. P. and Jack, K. H., The Fabrication of Composite O'-β' Sialon Ceramics. In: *Proc. Twenty-First Univ. Conf. on Ceramic Science, Tailoring Multiphase and Composite Ceramics*, Eds R. E. Tressler, G. L. Messing, C. G. Pantano and R. E. Newnham, 1986, 93-101.

4. Naik, I. K. and Tien, T. Y., Subsolidus Phase Relations in Part of the System Si, Al, Y/N, O, *J. Amer. Ceram. Soc.*, **62**(11–12) (1979) 642–3.
5. Cao, G. Z., Huang, Z. K, Fu, X. R. and Yan, D. S. (Yen, T. S.), Phase Equilibrium Studies in Si<sub>2</sub>N<sub>2</sub>O-containing System: 1, Phase Relations in the Si<sub>2</sub>N<sub>2</sub>O–Al<sub>2</sub>O<sub>3</sub>–Y<sub>2</sub>O<sub>3</sub> System, *Int. J. High Tech. Ceram.*, **1**(2) (1985) 119–27.
6. Boskovic, S., Gauckler, L. J., Petzow, G. and Tien, T. Y., Reaction Sintering Forming  $\beta$ -Si<sub>3</sub>N<sub>4</sub> Solid Solutions in the System Si, Al/N, O; 1, Sintering of SiO<sub>2</sub>–AlN Mixtures, *Powder Metallurgy International*, **9**(4), (1977) 185–9.
7. Huang, Z. K., Greil, P. and Petzow, G., Formation of  $\alpha$ -Si<sub>3</sub>N<sub>4</sub> Solid Solutions in the System Si<sub>3</sub>N<sub>4</sub>–AlN–Y<sub>2</sub>O<sub>3</sub>, *J. Amer. Ceram. Soc.*, **66**(6) (1983) 96–7.
8. Thompson, D. P., Sun, W. Y. and Walls, P. A.,  $O'$ – $\beta'$  and  $\alpha'$ – $\beta'$  Sialon Ceramics. In: *Proc. Second Int. Symp. on Ceramic Materials and Components for Engines*, 1986 Lübeck–Travemünde, FRG, Eds W. Bunk and H. Hausner, Deutsche Keramische Gesellschaft, 643–50.

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